

Introduction

Communication Satellite Frequency Allocation

Communication satellites operate within two frequency bands for TV/Broadband service broadcast signals, C Band and Ku Band. The C Band overall frequency spectrum is 4.0GHz - 8.0GHz, while the Ku Band overall frequency spectrum is 11.7GHz -18.0GHz.

Within these bands each satellite will have specific uplink and downlink frequency allocation. For example the North American DBS system has categories assigned as follows, Ku Band high power downlink is 12.2GHz –12.7GHz and 17.3GHz-17.8GHz as the uplink frequency, C Band downlink frequency is 3.7GHz to 4.2GHz and 5.925GHz-6.425GHz as uplink frequency.

Also, to use the frequencies that are available for satellite broadcast as efficiently as possible, and to accommodate additional number of channels within a given frequency band, the transmission signal can be formatted to be either vertical and horizontal, or circular right-hand and circular left-hand simultaneously per frequency.

What is a Low Noise Block (LNB)?

An LNB is a low noise block module, placed on the focus of the dish antenna (parabola) that provides the following functions:

- Down conversion of the incoming signal from GHz range to 910MHz -2150MHz (for Europe) range called “first conversion signal.” This conversion allows the signal to be carried by an inexpensive coaxial cable towards the receiver.
- Signal amplification with good noise factor. The LNB improves the first conversion signal level through the use of a built-in low noise amplifier.
- Selects Vertical or Horizontal polarization.
- Selects operating band by switching its internal oscillator from Low band to High band when it “receives” a 22kHz tone. Specifically the local oscillator (LO) frequency changes from 9.75GHz to 10.6GHz.
C Band - LO frequency 9.75GHz
Ku Band - LO frequency 10.6GHz
- Miscellaneous functions based on 22kHz tone PPM encoding, as discussed later in the paper.

Polarization Selection

Polarization is a way to give a transmission signal specific direction. It increases the beam concentration. The signal transmitted by satellite can be polarized in one of four different ways: Linear (horizontal or vertical) or Circular

(right-hand or left-hand). Consequently, the satellite can broadcast both H and V or LH and RH polarized signals via one frequency.

The “universal” LNB switches the polarization by looking at the voltage that it receives from the receiver.

12V – Horizontal, 18V – Vertical

13V – Circular right-hand, 20V – Circular left-hand

Generally, only two (12V and 18V or 13V and 20V) will be used with one type of Antenna. Also 1V can be added from a receiver to any of above voltages to compensate for the voltage drop in the coaxial cable, i.e., it could be 13V (12V), 14V (13V), 19V (18V) or 21V (20V) instead.

22kHz Tone and DiSEqC™ (Digital Satellite Equipment Control) Encoding

In addition to selecting the polarization, the LNB needs to select the operating band. This is done with the use of a 22kHz tone frequency. A 22kHz pulse-position modulated signal of about 0.6V amplitude is superimposed on the LNB’s DC power rail. Its coding scheme allows the remote electronics to perform more complex functions like varying the down conversion frequency to select one of multiple LNB’s for dual-dish systems or physically rotating the antenna assembly. Traditionally, when other encoding functions do not require using 22kHz tone, simple presence or absence of this tone selects the operating band by changing the local oscillator frequency of the LNB.

The complex encoding of 22kHz burst is done with a more sophisticated communication bus protocol named DiSEqC standard (Digital Satellite Equipment Control). The open DiSEqC standard developed by the European Telecommunication Satellite Organization is a well accepted worldwide standard for communication between satellite receivers and satellite peripheral equipment.

The 22kHz oscillator has to be a tone generator with specific rise and fall time. The wave shape will be a quasi-square wave. (Sine with flat-top). The required frequency tolerance is ± 2 kHz over line and temperature variations. Burst coding of this signal is accomplished by input from the microcontroller at the DSQIN pin of the IC as detailed in the datasheet.

22kHz WAVE SHAPE AND DETAILS (See Figures 1 and 2)

Carrier frequency: 22kHz ± 2 kHz over line and temperature

Carrier amplitude: 650mVpp ± 250 mV

Modulation mark period: 500 μ s ± 100 μ s

Modulation space period: 1ms ± 200 μ s

Methods of Modulation

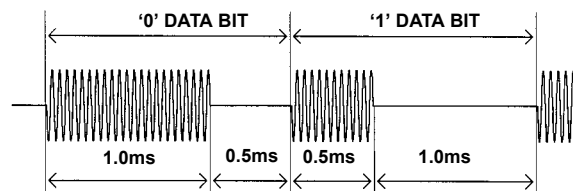


FIGURE 1. DiSEqC™ MODULATION SCHEME

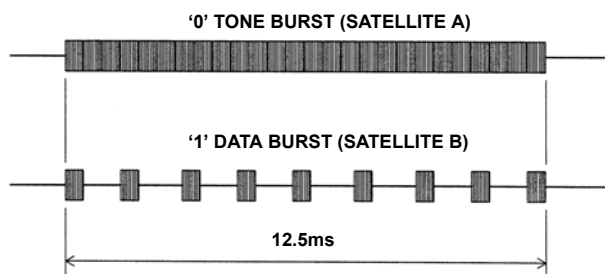


FIGURE 2. TIMING DIAGRAM FOR TONE BURST CONTROL SIGNAL

ISL6424 - Provides a Complete Power Solution for Dual LNB Control

The ISL6424 is a highly integrated solution for supplying power and control signals from advanced satellite set-top box (STB) modules to the low noise blocks (LNBs) of two antenna ports. This dual output device is comprised of two independent current-mode boost PWMs and two low-noise linear regulators along with the circuitry required for I²C device interfacing and for providing DiSEqC standard control signals to the LNB.

Regulator output voltages are available at two output terminals (VO1, VO2) to support simultaneous operation of two antenna ports in advanced satellite STBs. The regulator outputs for each PWM are set to 13V or 18V by independent voltage select commands (VSEL1, VSEL2) through the I²C bus. Additionally, to compensate for the voltage drop in the coaxial cable, the selected voltage may be increased by 1V with the line length compensation (LLC) feature. Separate enable commands sent on the I²C bus provide independent standby mode control for each PWM and linear combination, disabling the output to conserve power.

Both independent tracking current-mode boost converters provide the linear regulators with input voltages that are set to the output voltages, plus typically 1.2V dropout to insure minimum power dissipation across each linear regulator. This maintains constant voltage drops across each linear pass element while permitting adequate voltage range for tone injection.

Please refer to the ISL6424 datasheet, FN9175, for more information.

Quick Start Evaluation

Out Of The Box

The ISL6424 evaluation board is shipped in a “ready-to-test” state. The board requires an input voltage ranging from 8V to 14V and a 3.3V/5V supply. The use of an electronic load enables evaluation over a wide range of operating conditions. The evaluation kit also includes 5 samples of ISL6424EEB and ISL6424ER, a PC to I²C bus interface board (USB-I2CIO), PC to I²C bus software, a USB cable, and a connector cable to connect the USB-I2CIO board and the ISL6424EVAL board.

TABLE 1. ISL6424 EVALUATION BOARDS

BOARD NAME	IC	PACKAGE
ISL6424EVAL1C	ISL6424EEB	28-Ld SOIC
ISL6424EVAL2C	ISL6424ER	32-Ld QFN

Required Test Equipment

To fully test the ISL6424 chip functionality, the follow equipment is needed:

- 4 channel oscilloscope with probes
- 2 electronic loads
- 2 bench power supplies
- Precision digital multi-meters
- I²C bus read/write capability

Power and Load Connections

Refer to the ISL6424EVAL1 and 2 schematics, the reference designators will differ. The ISL6424EVAL1 evaluation board has four sets of terminal posts and three jumpers that are used to supply the input voltages and to monitor and load the outputs.

Jumper and Switch Settings - JP1, JP2, and JP3 will be shorted with shunt jumpers for quick start evaluation. JP1 and JP2 can be removed to monitor the input current for each boost regulator or the input bias current of the IC. JP3 sets the chip address to 0.

The control pins for DSQIN1, DSQIN2, SEL18V1, and SEL18V2 are available at respective terminal posts. These are by default in the low condition. They will have to be pulled high to activate the respective function.

Input Voltage - Adjust two power supplies to provide the 5V/3.3V and 12V input voltages of the evaluation board. With the power supplies turned off, connect the positive lead of the 12V supply to the VIN post (P1) and the ground lead to the GND post (P2).

The second supply set for either 5V or 3.3V provides the pull-up voltage for the I²C bus clock and data line. Connect the positive lead of the second supply to the +5V/+3.3V post (P5) and the ground lead to the GND post (P10-EVAL2).

Output Voltage Loading and Monitoring - To exercise and monitor VOUT1, connect the positive lead of one of the electronic loads and the positive lead of a digital multimeter to the VOUT1 post (P3) and the ground lead to the GND post (P4).

To exercise and monitor VOUT2, connect the positive lead of one of the electronic loads and the positive lead of a digital multimeter to the VOUT2 post (P8) and the ground leads of both to the GND post (P10).

I²C Bus Communication Setup

To control and exercise the ISL6424 requires communication through the I²C bus clock (SCL) and data (SDA) pins. Refer to the ISL6424 datasheet for more information about the I²C bus specification. You can use the existing I²C hardware/software, a word generator, or the PC to I²C hardware/software included in the ISL6424 evaluation kit to produce the necessary I²C waveforms.

USB-I²CIO Board Driver Installation - To use a PC to control the I²C bus to communicate with the ISL6424 you will have to install the drivers of the USB-I²CIO board included in the kit. You will need a Windows 98/XP/2000 machine with a standard USB port.

1. The evaluation kit comes with a CD containing the software and drivers to control the I²C bus. Copy the contents of the CD to some directory, e.g., C:\some directory'.
2. Applying power to the USB-I²CIO board: The USB-I²CIO board has the option of being powered with 3.3V through the USB bus of the PC or externally with 5V connected to the +5 test point and GND test point. The I²C bus can operate at 3.3V or 5V logic. If you use external 5V then place a shunt jumper shorting pins 2 and 3 of JP3. If you are using an external 5V to power the USB-I²CIO board place a shunt jumper shorting pins 1 and 2 of JP3.
3. After the USB-I²CIO board is powered up, connect the USB cable to the USB port of a PC.
4. Windows should detect the new USB device and the 'Found New Hardware Wizard' should begin. This will help you install the drivers. Follow the directions on the screen until it asks you where to search for the drivers. At this point, you should select the 'choose location' option and browse to the C:\some directory' created in step one and select the drivers folder.
5. Follow the remaining directions and the driver should be installed and the USB-I²CIO detected by your PC.
6. If this is successful, another 'Found New Hardware Wizard' window will appear. Repeat steps 4 and 5. At this point, the USB-I²CIO board should be ready to use.
7. To connect the USB-I²CIO board to the ISL6424 evaluation board, use the 5-pin to 4-pin connector cable. Connect the 5-pin connector to J4 on the USB-I²CIO board and the 4-pin connector to J3 on the ISL6424 evaluation board. Figure 3 and 4 show the test setup configuration to evaluate the ISL6424 evaluation boards.

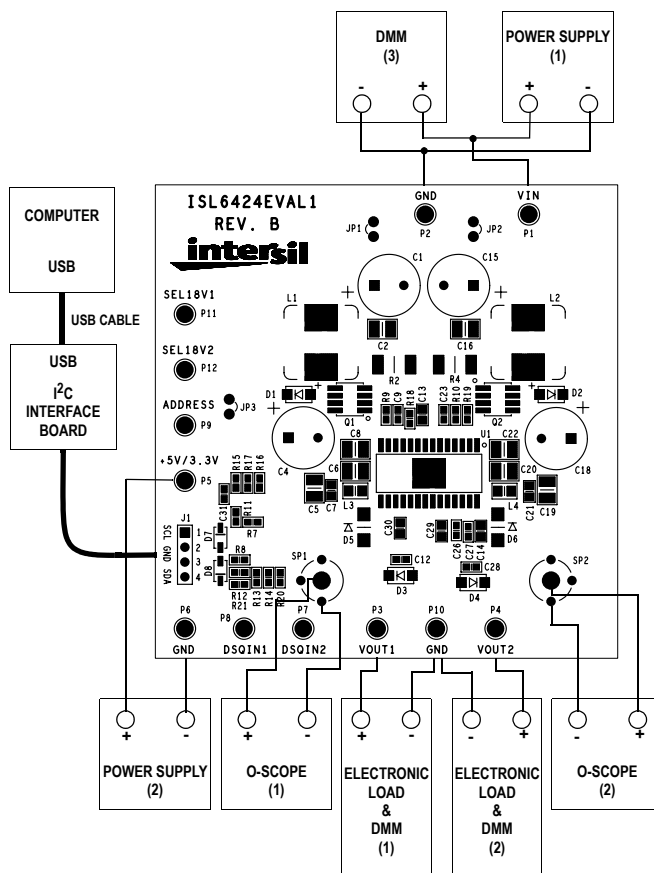


FIGURE 3. ISL6424EVAL1 TEST SETUP

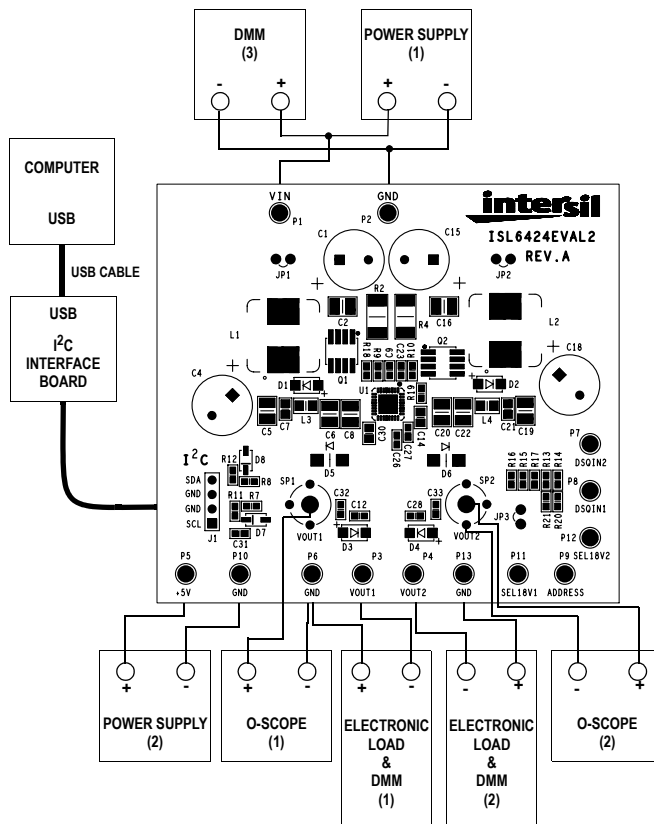


FIGURE 4. ISL6424EVAL2 TEST SETUP

8. Turn on the power supplies to power up the ISL6424 evaluation board.
9. Run the ISL6424i2crevb.exe program copied to C:\'some directory'. Figure 5 shows the PC to I²C software application window. Click the 'Open Device' button.
10. If you receive a 'No USB Device Detected' error:
 - Make sure the drivers were installed correctly. If Windows did not detect your USB device, try running the Add/Remove Hardware Wizard in the control panel.
 - Make sure the USB board is powered up (internally or externally, not both).
11. If you receive the 'Incorrect Return Value' error:
 - The ISL6424 evaluation board may not be powered up. Check the power connections.
 - Make sure SCL and SDA are connected correctly. The 5-pin connector to the USB-I²CIO board only fits one way. Try reversing the 4-pin connector at J3 of the ISL6424 evaluation board.

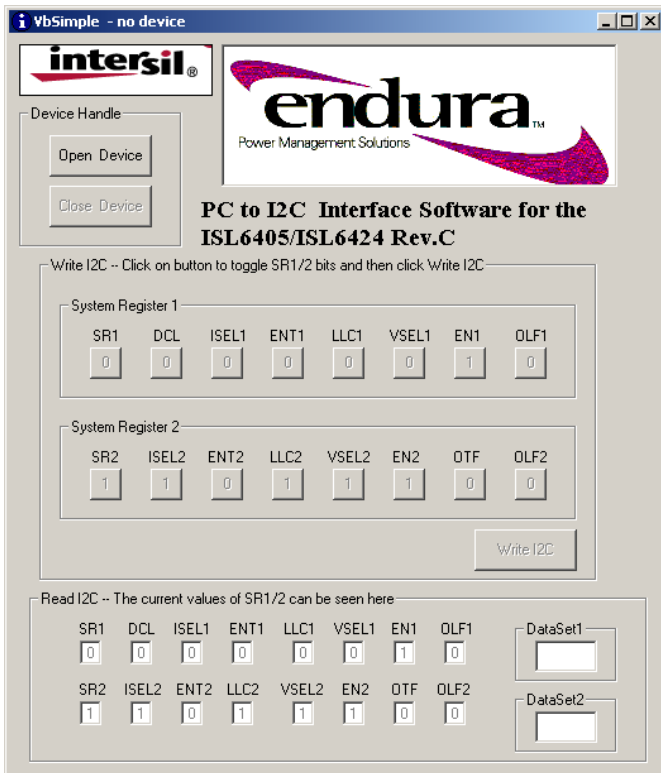


FIGURE 5. PC TO I²C APPLICATION WINDOW

Using the PC to I²C Application

After opening the application window and clicking on the 'Open Device' button, the program will detect the USB-I²CIO board and initialize the I²C system registers of the ISL6424. To evaluate the ISL6424 functionality, toggle the system register bits as needed and then click on the 'Write I²C' button to write to the system registers. The lower portion of the application window shows the current values of the

system register bits. They are read and updated continuously. The OLF1/2 and OTF flag in system register 1 and 2 are read only bits and they provide diagnostic status of the ISL6424.

The switch, SW1, allows you to change the I²C address of the ISL6424 by toggling the ADDR pin high or low. With the switch in its default position the ADDR pin is low. The application software will not be able to communicate with the ISL6424 if the ADDR pin is high.

Performance Characterization

Startup

The ISL6424 features internal soft-start to reduce external number of components. Figure 6 shows typical soft-start waveform. Typical soft-start time is 4.6ms.

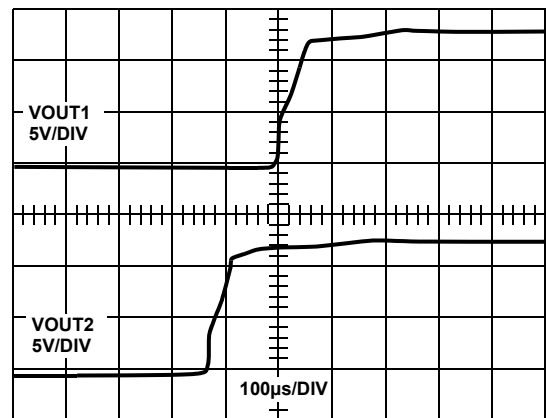


FIGURE 6. SOFT-START

Shutdown

Both LNB outputs of ISL6424 can be independently shutdown using ENx bits via I²C. Figure 7 shows typical shutdown waveforms.

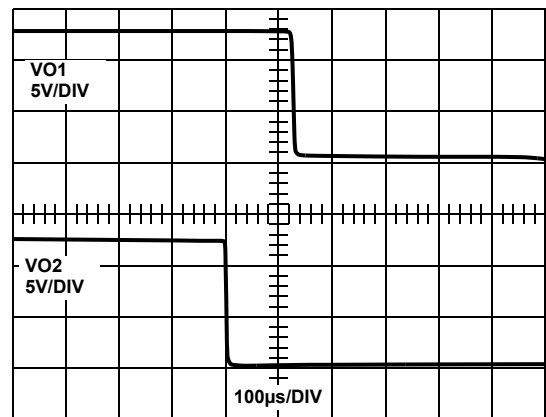


FIGURE 7. SHUTDOWN USING I²C ENABLE

Boost PWM Efficiency

The Boost PWM architecture allows close to 90% efficiency at full load as shown in Figure 8.

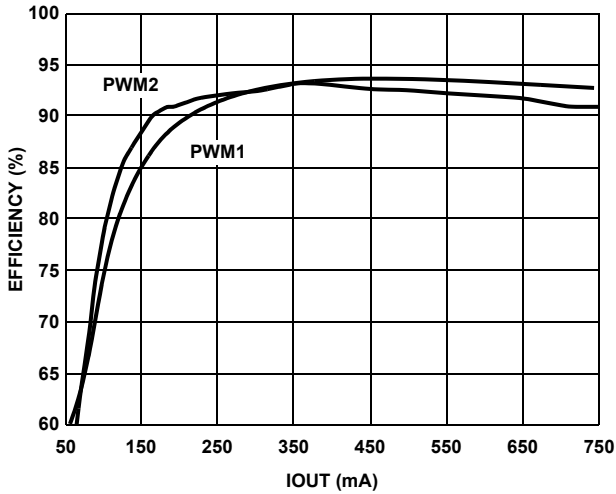


FIGURE 8. BOOST PWM1 AND PWM2 EFFICIENCY vs LOAD

DiSEqC Implementation

The ISL6424 has a built-in 22kHz tone generator that can be controlled either by the I²C interface or by a dedicated pin (DSQIN) that allows immediate DiSEqC data encoding for the DiSEqC compliance. When the I²C tone enable bit (ENT) is set to HIGH, a continuous 22kHz tone is generated regardless the status of the DSQIN pin. The ENT pin must be LOW when DSQINx pins are being used for DiSEqC encoding. Figure 9 shows the 22kHz tone waveform with 350mA load.

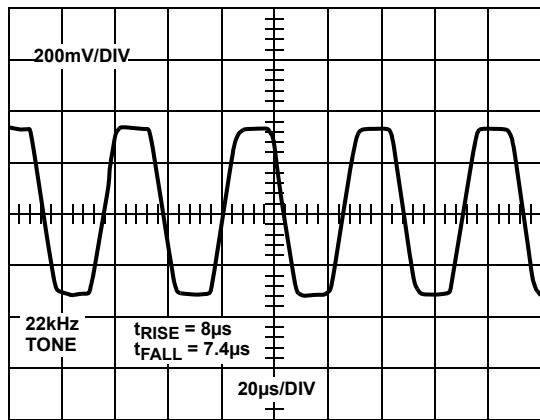


FIGURE 9. 22kHz TONE OPERATION

Overcurrent Hiccup Mode

Figure 10 shows a typical overcurrent trip.

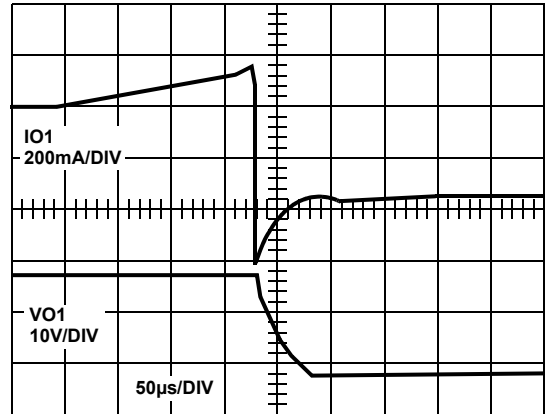


FIGURE 10. OVERCURRENT TRIP

When the DCL (dynamic current limiting) bit is set LOW, the overcurrent protection circuit works dynamically; as soon as an overload is detected, the output is shutdown for a time t_{OFF}, typically 900ms. The output is resumed for a time t_{ON} = 20ms. At the end of t_{ON}, if the overload condition is still detected, the protection circuit will cycle again through t_{OFF} and t_{ON}. Figure 12 shows the typical waveforms for the overcurrent hiccup mode.

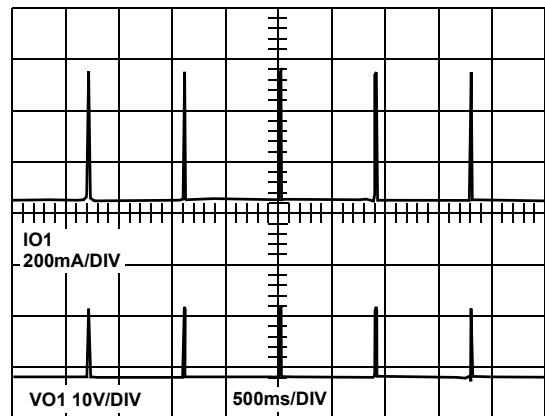


FIGURE 11. OVERCURRENT HICCUP MODE

Output Ripple

Figure 12 shows the typical output ripple waveforms. VO1 is set to 19V and 750mA load. VO2 is set to 13V and 350mA load.

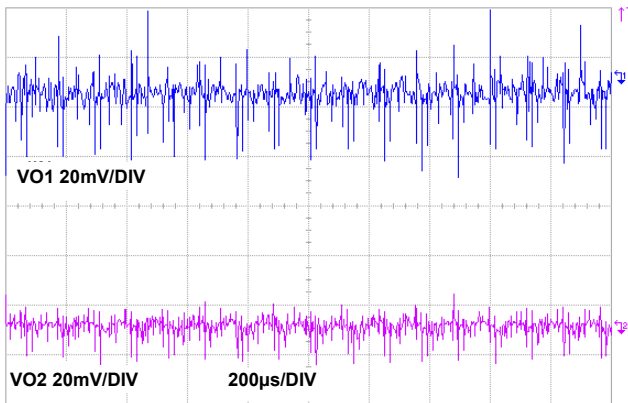


FIGURE 12. OUTPUT RIPPLE

External Back-Bias Protection

Some applications may need to be able to protect the ISL6424 from an inadvertent back-bias voltage condition. For the case where a 24V supply is connected to the output of the ISL6424, a series connected diode as shown in Figure 13 will protect the IC. The LLC bit can be set high through the I²C bus to increase the output voltage by 1V to compensate for the diode voltage drop.

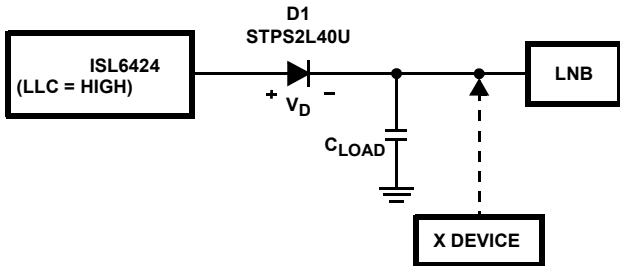


FIGURE 13. DC BACK-BIAS PROTECTION CIRCUIT

The DiSEqC standard recommends a maximum bus load of 0.25µF. For the circuit in Figure 13 to provide proper 22kHz tone operation, the bus would have to have a minimum loading of 12mA.

If tone operation is required at zero load conditions, a resistor can be placed from the cathode of the protection diode to ground, scaled to provide the minimum 12mA. To avoid the added dissipation of this method, a capacitor can be placed in parallel with the back-bias protection diode as shown in Figure 14. This capacitor should be scaled with the capacitive load present on the DiSEqC bus line. For a load of 0.25µF, use a 10µF capacitor. Consider the maximum load of 0.25µF and the highest output voltage of 19V and a 0.5V drop across the Schottky diode. After the tone rise time, $Q_d(\text{rise}) \sim 0$, $Q_{\text{load}}(\text{rise}) = 19V \cdot 0.25\mu F = 4750nC$.

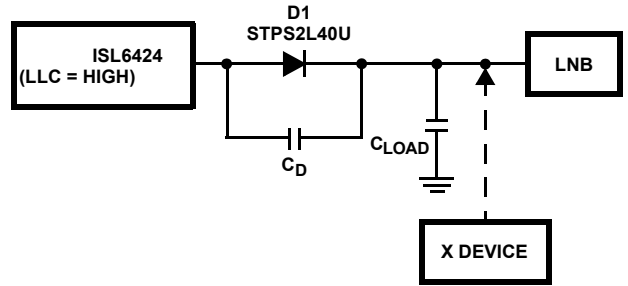


FIGURE 14. DC BACK-BIAS PROTECTION CIRCUIT FOR ZERO LOAD CONDITION

During the tone fall time, the capacitors are essentially in series so the charge will try to equally distribute between C_d and C_{load}. C_{load} will discharge allowing current to flow to C_d to match the falling voltage at the anode of the diode. You will have to choose a capacitor, C_d, that is large enough to absorb the C_{load} discharging current and to minimize the voltage drop created during the minimum tone fall time specification, 5µs. A good choice would be to use a capacitor for C_d that is 4 times the value of C_{load}.

Figure 15 shows the tone mode operation at the cathode of the protection diode in a zero load condition and the charging current between C_d and C_{load}. Excessive current transients may occur from a fast dV/dt created if a 24V supply were connected to the output of the ISL6424, therefore, to use the circuit in Figure 14, the 24V supply would have to be limited to 1A maximum current considering the dV/dt voltage transient, to fully protect the IC.

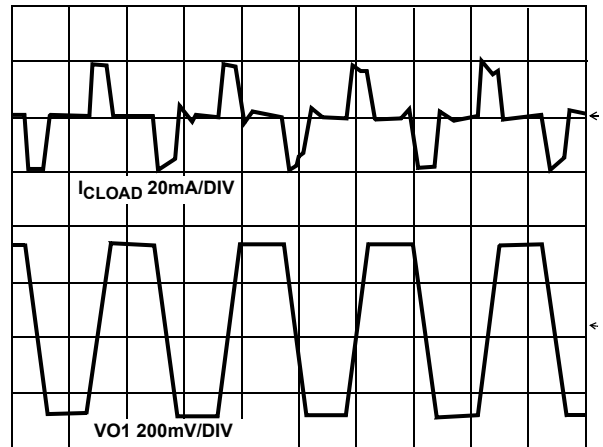


FIGURE 15. ZERO LOAD 22kHz TONE AT CATHODE OF DIODE AND DRIVING CURRENT CHARGING AND DISCHARGING CLOAD

Component Selection Guidelines

The ISL6424EVAL application schematics show the configuration for a dual LNB power supply.

TCAP Capacitor

A capacitor connected to the TCAP pin sets the transition time from 13V to 18V. A minimum 1µF capacitor is required for smooth transition with reduced peak currents. Figure 16 shows the transition time versus capacitor value.

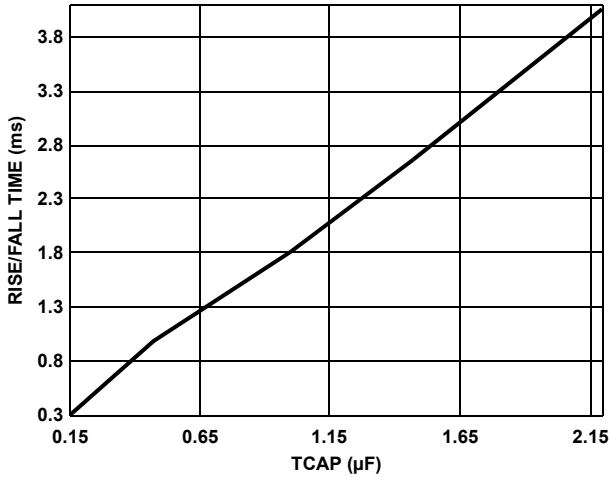


FIGURE 16. TCAP CAPACITOR VALUE vs OUTPUT TRANSITION TIME

The programmed output voltage rise and fall times can be set by an external capacitor. The output rise and fall times will be approximately 3400 times the TCAP value. For the recommended range of 0.47µF to 2.2µF, the rise and fall time would be 1.6ms to 7.6ms. Use of a 0.47µF capacitor insures the PWM will stay below its overcurrent threshold when charging a 120µF VSW filter cap during the worst case 13V to 19V transition. This feature only affects the turn-on and programmed voltage rise and fall times. Figure 17 shows the 13V to 18V transition with TCAP=1µF.

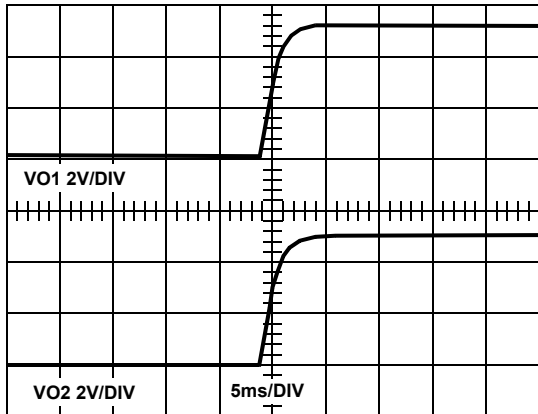


FIGURE 17. 13V TO 18V TRANSITION

Inductor

The ISL6424 operates with a 33µH standard inductor over the entire range of supply voltages and load currents. Choose an inductor that can handle at least the peak switch current without saturating, and ensure that the inductor has a low DCR (series resistance) to maximize efficiency. The inductor saturation current must be greater than the switch peak current,

$$I_{PEAK} = \frac{V_{SW(max)} \cdot I_{OUT}}{N \cdot V_{IN(min)}} + \frac{V_{IN(min)}}{2L \cdot f_{SW}} \left(1 - \frac{V_{IN(min)}}{V_{SW(max)}} \right) \quad (EQ. 1)$$

where,

L = Inductance 33µH

f_{SW} = PWM switching frequency, 220kHz Typical

N = Efficiency, 92% at maximum load

TABLE 2. RECOMMENDED INDUCTORS

VENDOR	PART NUMBER	ISAT (A)	DCR (mΩ)	PACKAGE
Coilcraft	MSS1260-333MX	2.2	75	SMD
Falco	SD1016	2.8	66	SMD

Output Capacitors

The most important parameter for the output capacitors is effective series resistance (ESR). The output ripple is directly proportional to output capacitor ESR value.

A 68µF or less aluminum output filter capacitor with ESR lower than 80mΩ in parallel with a 470nF ceramic capacitor is a good choice in most application conditions. A ceramic capacitor is necessary to reduce the high frequency switching noise.

A high output capacitance and low ESR will strongly reduce the output ripple voltage, output switching noise and improve efficiency. Use the lowest possible ESR capacitor for best performance.

The maximum value output capacitor is restricted by transition time specifications between 13V to 18V. With a high output capacitor the boost circuit will need higher peak current from input supply to make transition from 13V to 18V in a given transition time as set by TCAP value. The Figure 16 shows the TCAP capacitor value versus transition time. Use high TCAP capacitor value for high output capacitors to allow sufficient time to charge the output capacitors in maximum load conditions.

The capacitor's voltage rating should be at least 35V, but higher voltage electrolytic capacitors generally have lower ESR numbers, and for this reason, to improve efficiency and output ripple, select a capacitor with higher voltage ratings.

TABLE 3.

VENDOR	SERIES	PACKAGE
Sanyo	OS-CON Electrolytic	SMD/Through hole
Panasonic	EEUFC Electrolytic	TH

Static Current Limit

The current sense resistor R_{sc} serves to set the peak current through the FET when in the static current limit mode. This resistor value is calculated based on peak switch current per Equation 2,

$$R_{SC} < \frac{V_{SENSE}}{I_{PEAK}} \quad (EQ. 2)$$

Where V_{sense} is 450mV typ. (See datasheet specification table) and I_{peak} is calculated from Equation 1. Make sure the R_{sc} value is always lower than the V_{sense}/I_{peak} ratio.

In the typical application conditions ($V_{CC} = 12V$, $I_{PEAK} (max) = 4500mA$) a 100m Ω R_{sc} value is a good choice.

If $V_{IN} < 10.5V$ the inductor peak current can be close to 2.5A. In the worst case with $V_{IN} = 8V$, and $I_{OUT} = 500mA$, low cost axial through-hole resistors could also be used, however, these are usually bigger and need a larger area on the PCB. See Table 4 for some suggested SMD resistor part numbers.

TABLE 4.

VENDOR	SERIES
KOA	SR73 3A
SEI Electronics	RMC1
Panasonic	ERJ L1W

Layout Guidelines

Just like all switching power supplies, a proper PC board layout is very important for a dual channel ISL6424 based power supply implementation. Protect sensitive analog grounds by using a star ground configuration. Also, minimize lead lengths to reduce stray capacitance, trace resistance, and radiated noise. Minimize ground noise by connecting PGND1/2, the input bypass capacitor ground lead, and the output filter capacitor ground lead to a single point. Place bypass capacitors as close as possible to BYP pin and PGND1/2 and the DC/DC output capacitors as close as possible to VSW1/2.

Place TCAP1/2 capacitors very close to the IC pins and have shortest possible ground return path.

Thermal Design

During normal operation, the ISL6424 dissipates some power. The power dissipation of the output linear regulator dominates the total power dissipated in the ISL6424. At the maximum rated output current, the voltage drop on the linear

regulator leads to a total dissipated power that is about $1.2V \times 750mA \times 2 = 1.8W$. At 350mA maximum current, this power will be $1.2V \times 350mA \times 2 = 0.84W$. The heat needs to be removed with a heatsink to keep the junction temperature below the over-temperature threshold.

The simplest solution is to use a large, continuous copper area of the ground layer to dissipate the heat. This area can be the inner ground of multi-layered pcbs, or in a dual layer pcb, or an unbroken ground area on the opposite side of the board where the IC is placed. In both cases, the thermal path between the IC ground pins and the dissipating copper area must exhibit a low thermal resistance.

The EPAD SOIC package of the ISL6424 has $\theta_{JA} = 27^{\circ}C/W$ and $\theta_{JC} = 2^{\circ}C/W$. The QFN package has $\theta_{JA} = 32^{\circ}C/W$ and $\theta_{JC} = 4^{\circ}C/W$. Due to the presence of exposed pad connected to ground below the IC body on both the EPAD SOIC and the QFN packages, the θ_{JC} is much lower. As a result, a much smaller copper area is required to dissipate heat than standard SOIC packages.

Conclusion

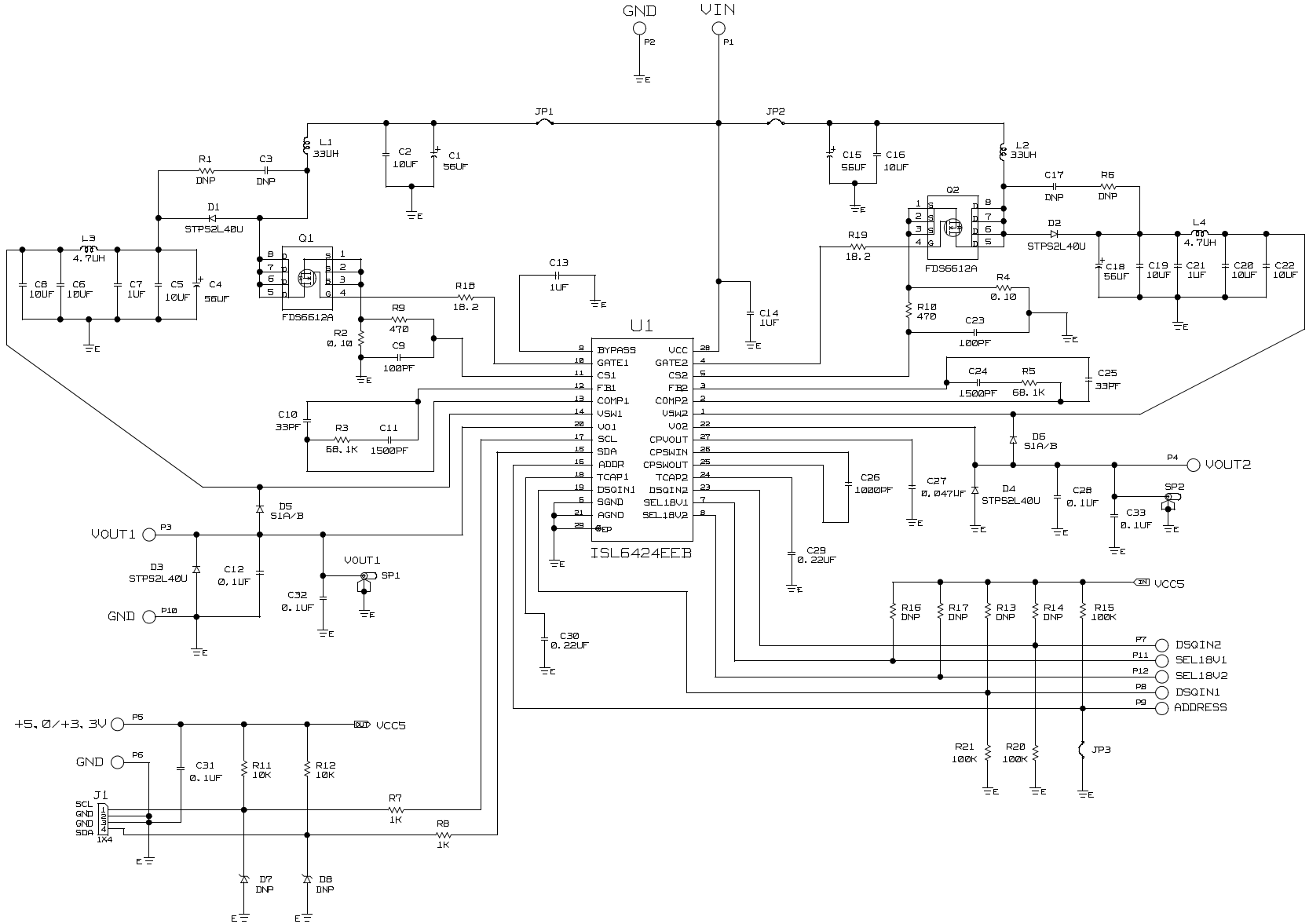
The ISL6424 dual output voltage regulator makes an ideal choice for advanced satellite set-top box and personal video recorder applications. The ISL6424EVAL1 and ISL6424EVAL2 are complete reference designs for providing power and control functions to the LNB in advanced satellite set-top box applications.

References

Intersil documents are available on the web at <http://www.intersil.com>.

- [1] *ISL6424 Data Sheet*, Intersil Corporation, File No. FN9175
- [2] *DiSEqC Bus Functional Specification*, EUTELSAT <http://www.eutelsat.com/docs/diseqc>
- [3] More information on the USB-I2CIO PC to I²C interface board available at <http://www.DeVaSys.com>

ISL6424 EVAL1 Rev B Schematic



Application Note 1177

Bill of Materials ISL6424EVAL1 Rev. B

ITEM	REFERENCE	QTY	PART NUMBER	PART TYPE	DESCRIPTION	PACKAGE	VENDOR
1	U1	1	ISL6424EEB	IC, Linear	Current mode PWM Controller	28 SOIC	Intersil
2	Q1, Q2	2	FDS6612A	MOSFET Single	N-channel, 30V, 0.022Ω, 8.4A	SOIC8	Fairchild
3	D1, D2, D3, D4	4	STPS2L40U	Diode, Schottky, Low Drop Power	Schottky, 30V, 2A	DO-214AA	STMicroelectronics
4	D5, D6	2	S1A/B	Diode, Rectifying	Rectifying, 50V	SMB	Diodes Inc.
5	D7, D8 (DNP)	0	BZT52C5V6	Diode, Zener	Zener, 5.6V, 500mW	SOD123	Diodes Inc.
6	L1, L2	2	MSS-1260-333MX	Inductor	33μH, 20%, 2.2A	MSS1260	CoilCraft
7	L3, L4	2	1008PS-472K	Inductor	4.7μH, 10%, 1.0A	SM	CoilCraft
CAPACITORS							
8	C1, C4, C15, C18	4	25SP56M	Capacitor, Aluminum	56μF, 20%, 25V	CASE-CC	Sanyo
9	C2, C5, C6, C8, C16, C19, C20, C22	8	C3225X7R1E106M	Capacitor, Ceramic, X7R	10μF, 20%, 25V	SM_1210	TDK/Generic
10	C3, C17	2	DNP			SM_0603	TDK/Generic
11	C7, C13, C14, C21	4	C2012X7R1E105K	Capacitor, Ceramic, X7R	1.0μF, 10%, 25V	SM_0805	TDK/Generic
12	C9, C23	2	C1608X7R1H101K	Capacitor, Ceramic, X7R	100pF, 10%, 50V	SM_0603	TDK/Generic
13	C10, C25	2	C1608COG1H330K	Capacitor, Ceramic, COG	33pF, 10%, 50V	SM_0603	TDK/Generic
14	C11, C24	2	C1608X7R1H152K	Capacitor, Ceramic, X7R	1500pF, 10%, 50V	SM_0603	TDK/Generic
15	C12, C28, C31, C32, C33	5	C1608X7R1H104K	Capacitor, Ceramic, X7R	0.1μF, 20%, 50V	SM_0603	TDK/Generic
16	C26	1	C1608X7R1H102K	Capacitor, Ceramic, X7R	1000pF, 10%, 50V	SM_0603	TDK/Generic
17	C27	1	C1608X7R1H473K	Capacitor, Ceramic, X7R	0.047μF, 10%, 50V	SM_0603	TDK/Generic
18	C29, C30	2	C2012X7R1E224K	Capacitor, Ceramic, X7R	0.22μF, 10%, 25V	SM_0603	TDK/Generic
RESISTORS							
19	R1, R6 (DNP)	0	DNP	Resistor, Film		SM_0603	Panasonic/Generic
20	R2, R4	2		Resistor, Power metal strip	0.1Ω, 1%, 1W	SM_2512	Panasonic/Generic
21	R3, R5	2		Resistor, Film	68.1kΩ, 1%, 0.1W	SM_0603	Panasonic/Generic
22	R7, R8	2		Resistor, Film	1kΩ, 1%, 0.1W	SM_0603	Panasonic/Generic
23	R9, R10	2		Resistor, Film	470Ω, 1%, 0.1W	SM_0603	Panasonic/Generic
24	R11, R12	2		Resistor, Film	10kΩ, 5%, 0.1W	SM_0603	Panasonic/Generic
25	R13, R14, R16, R17 (DNP)	4	DNP	Resistor, Film		SM_0603	Panasonic/Generic
26	R15, R20, R21	3		Resistor, Film	100kΩ, 5%, 0.1W	SM_0603	Panasonic/Generic
27	R18, R19	2		Resistor, Film	18.2Ω, 1%, 0.1W	SM_0603	Panasonic/Generic

Application Note 1177

Bill of Materials ISL6424EVAL1 Rev. B (Continued)

ITEM	REFERENCE	QTY	PART NUMBER	PART TYPE	DESCRIPTION	PACKAGE	VENDOR
OTHERS							
28	J1	1	22-03-2041	Connector	Header Strip, 1X4	1x4 @ .1"	Molex
29	JP1, JP2, JP3	3	68000-236-1X2	Header	1X2 Break Strip GOLD		
30	JP1, JP2, JP3	3	S9001-ND	Jumper	2 pin jumper		Digikey
31	SP1, SP2	2	131-4353-00	Terminal, Scope Probe	Terminal, Scope Probe		Tektronix
32	P1 - P12	12	160-2043-02-01-00	Turret Post	Terminal post, through hole	PTH	Cambion
33		4		Bumpers			

ISL6424EVAL1 Rev B Layout

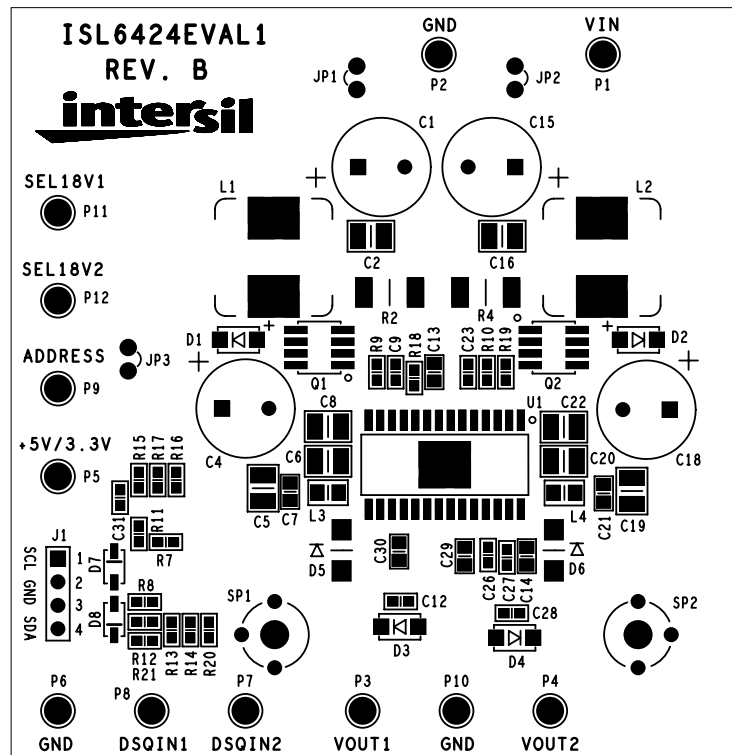


FIGURE 18. TOP SILKSCREEN

ISL6424EVAL1 Rev B Layout (Continued)

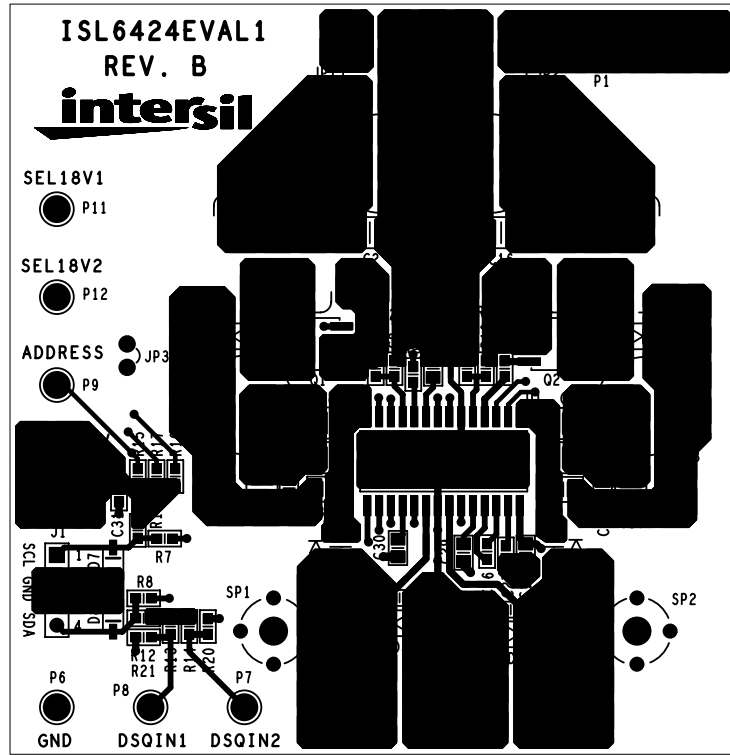


FIGURE 19. LAYER 1

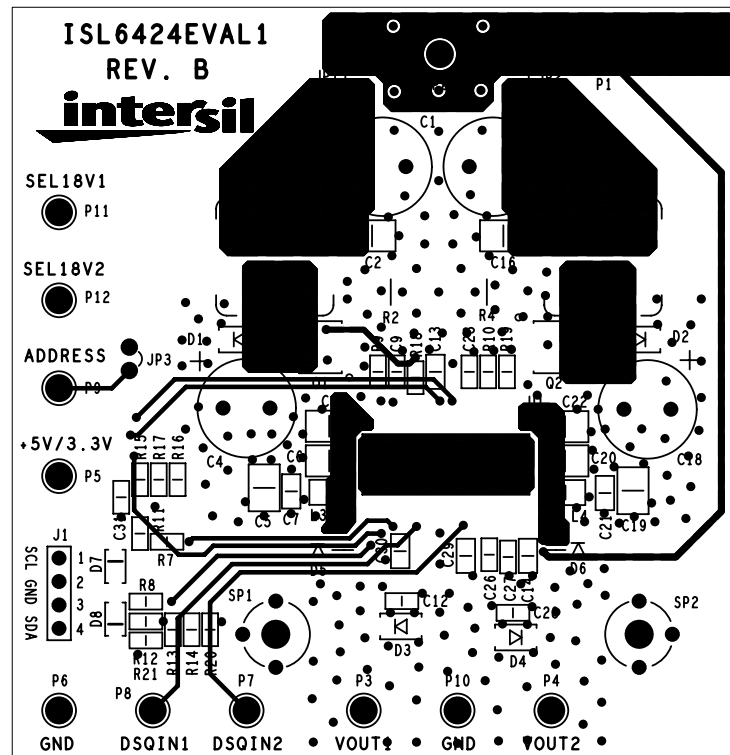


FIGURE 20. LAYER 2

ISL6424EVAL1 Rev B Layout (Continued)

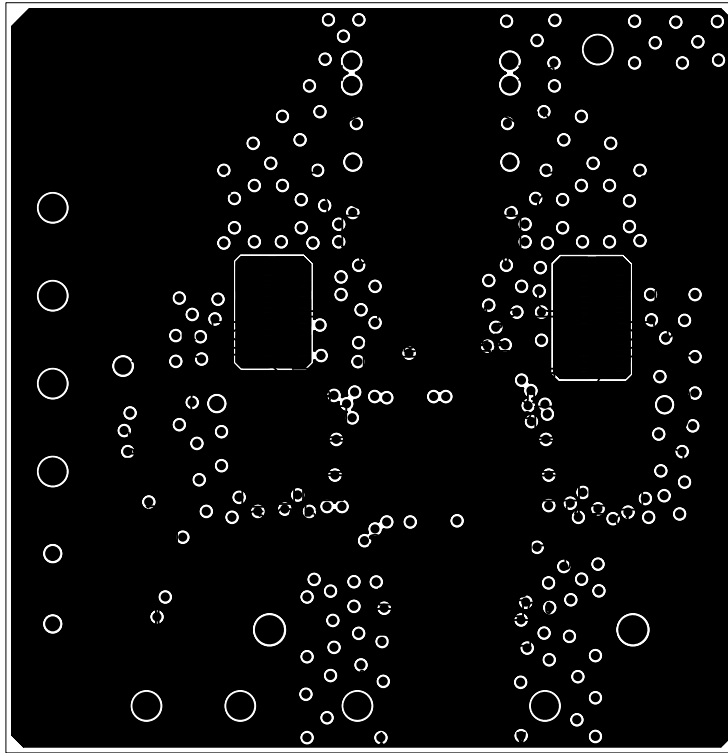


FIGURE 21. LAYER 3

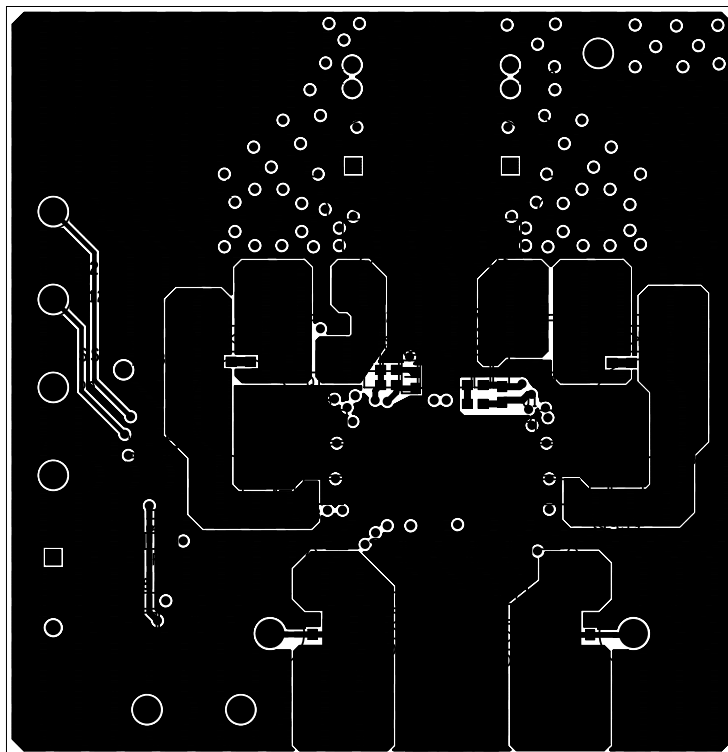


FIGURE 22. LAYER 4

ISL6424EVAL1 Rev B Layout (Continued)

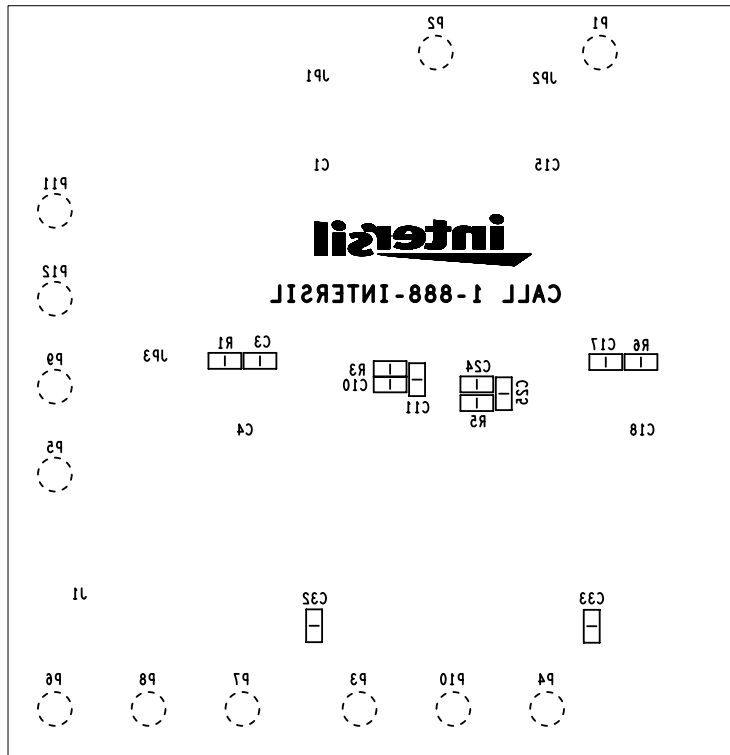
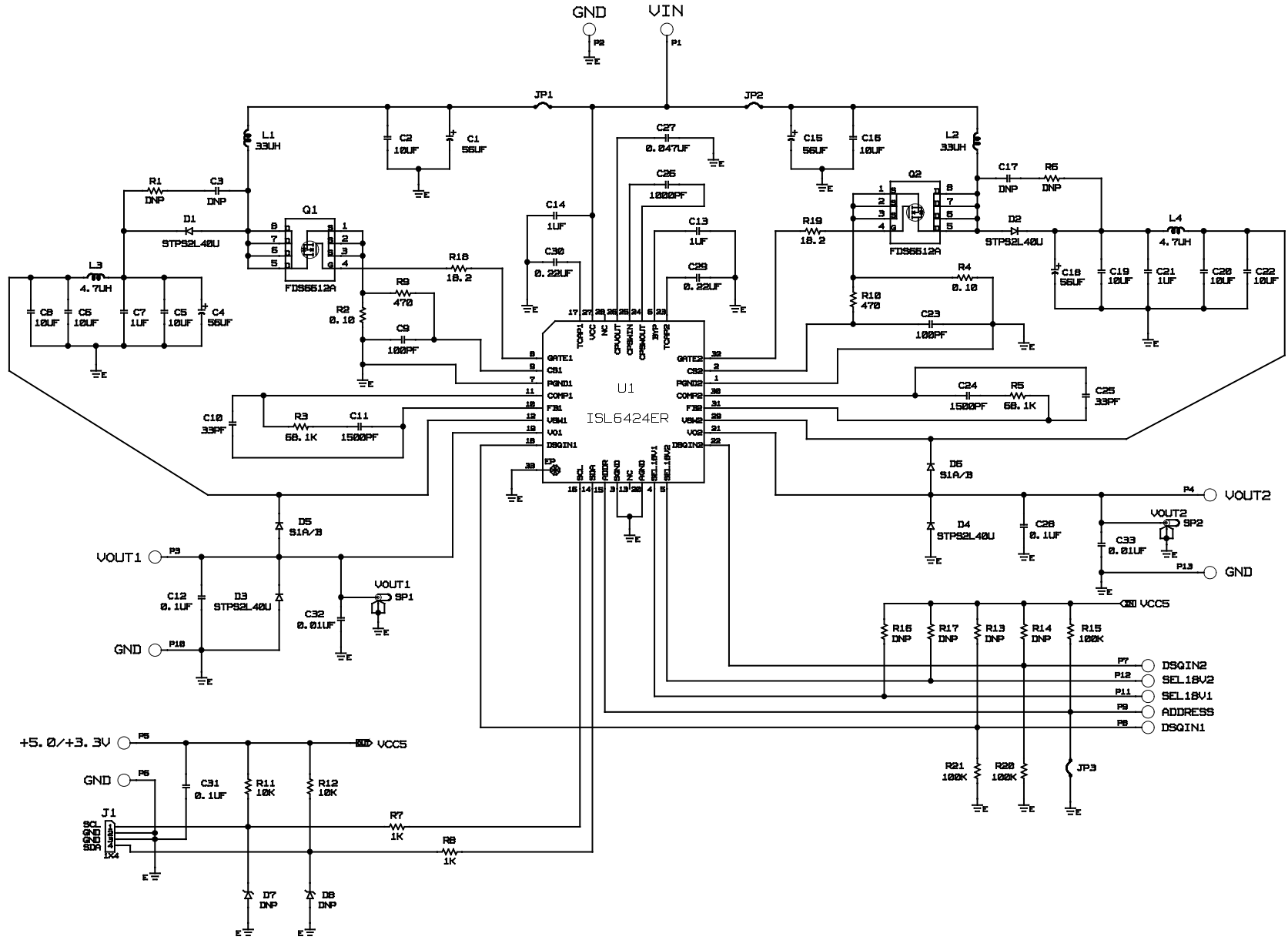


FIGURE 23. BOTTOM SILKSCREEN

ISL6424 EVAL2 Schematic Diagram



Application Note 1177

Bill of Materials ISL6424EVAL2 Rev. A

ITEM	REFERENCE	QTY	PART NUMBER	PART TYPE	DESCRIPTION	PACKAGE	VENDOR
1	U1	1	ISL6424ER	IC, Linear	Current mode PWM Controller	32LD QFN (5x5)	Intersil
2	Q1, Q2	2	FDS6612A	MOSFET Single	N-channel, 30V, 0.022Ω, 8.4A	SOIC8	Fairchild
3	D1, D2, D3, D4	4	STPS2L40U	Diode, Schottky, Low Drop Power	Schottky, 30V, 2A	DO-214AA	STMicroelectronics
4	D5, D6	2	S1A/B	Diode, Rectifying	Rectifying, 50V	SMB	Diodes Inc.
5	D7, D8 (DNP)	0	BZT52C5V6	Diode, Zener	Zener, 5.6V, 500mW	SOD123	Diodes Inc.
6	L1, L2	2	MSS-1260-333MX	Inductor	33μH, 20%, 2.2A	MSS1260	CoilCraft
7	L3, L4	2	1008PS-472K	Inductor	4.7μH, 10%, 1.0A	SM	CoilCraft
CAPACITORS							
8	C1, C4, C15, C18	4	25SP56M	Capacitor, Aluminum	56μF, 20%, 25V	CASE-CC	Sanyo
9	C2, C5, C6, C8, C16, C19, C20, C22	8	C3225X7R1E106M	Capacitor, Ceramic, X7R	10μF, 20%, 25V	SM_1210	TDK/Generic
10	C3, C17	2	DNP			SM_0603	TDK/Generic
11	C7, C13, C14, C21	4	C2012X7R1E105K	Capacitor, Ceramic, X7R	1.0μF, 10%, 25V	SM_0805	TDK/Generic
12	C9, C23	2	C1608X7R1H101K	Capacitor, Ceramic, X7R	100pF, 10%, 50V	SM_0603	TDK/Generic
13	C10, C25	2	C1608COG1H330K	Capacitor, Ceramic, COG	33pF, 10%, 50V	SM_0603	TDK/Generic
14	C11, C24	2	C1608X7R1H152K	Capacitor, Ceramic, X7R	1500pF, 10%, 50V	SM_0603	TDK/Generic
15	C12, C28, C31	3	C1608X7R1H104K	Capacitor, Ceramic, X7R	0.1μF, 10%, 50V	SM_0603	TDK/Generic
16	C26	1	C1608X7R1H102K	Capacitor, Ceramic, X7R	1000pF, 10%, 50V	SM_0603	TDK/Generic
17	C27	1	C1608X7R1H473K	Capacitor, Ceramic, X7R	0.047μF, 10%, 50V	SM_0603	TDK/Generic
18	C29, C30	2	C2012X7R1E224K	Capacitor, Ceramic, X7R	0.22μF, 10%, 25V	SM_0603	TDK/Generic
19	C32, C33	2	C1608X7R1H103K	Capacitor, Ceramic, X7R	0.01μF, 10%, 50V	SM_0603	TDK/Generic
RESISTORS							
20	R1, R6 (DNP)	0	DNP	Resistor, Film		SM_0603	Panasonic/Generic
21	R2, R4	2		Resistor, Power metal strip	0.1Ω, 1%, 1W	SM_2512	Panasonic/Generic
22	R3, R5	2		Resistor, Film	68.1kΩ, 1%, 0.1W	SM_0603	Panasonic/Generic
23	R7, R8	2		Resistor, Film	1kΩ, 1%, 0.1W	SM_0603	Panasonic/Generic
24	R9, R10	2		Resistor, Film	470Ω, 1%, 0.1W	SM_0603	Panasonic/Generic
25	R11, R12	2		Resistor, Film	10kΩ, 5%, 0.1W	SM_0603	Panasonic/Generic
26	R13, R14, R16, R17 (DNP)	4	DNP	Resistor, Film		SM_0603	Panasonic/Generic
27	R15, R20, R21	3		Resistor, Film	100kΩ, 5%, 0.1W	SM_0603	Panasonic/Generic
28	R18, R19	2		Resistor, Film	18.2Ω, 1%, 0.1W	SM_0603	Panasonic/Generic
OTHERS							
29	J1	1	22-03-2041	Connector	Header Strip, 1X4	1x4 @ .1"	Molex
30	JP1, JP2, JP3	3	68000-236-1X2	Header	1X2 Break Strip GOLD		

Application Note 1177

Bill of Materials ISL6424EVAL2 Rev. A (Continued)

ITEM	REFERENCE	QTY	PART NUMBER	PART TYPE	DESCRIPTION	PACKAGE	VENDOR
31	JP1, JP2, JP3	3	S9001-ND	Jumper	2 pin jumper		Digikey
32	SP1, SP2	2	131-4353-00	Terminal, Scope Probe	Terminal, Scope Probe		Tektronix
33	P1 - P12	12	160-2043-02-01-00	Turret Post	Terminal post, through hole	PTH	Cambion
34		4		Bumpers			

ISL6424EVAL2 Layout

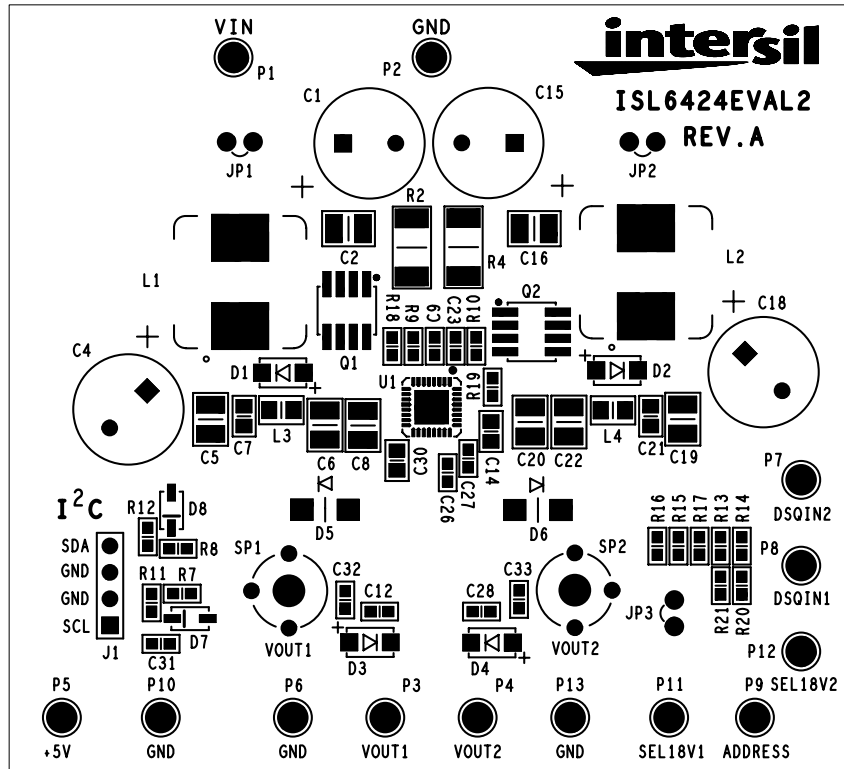


FIGURE 24. TOP SILKSCREEN

ISL6424EVAL2 Layout (Continued)

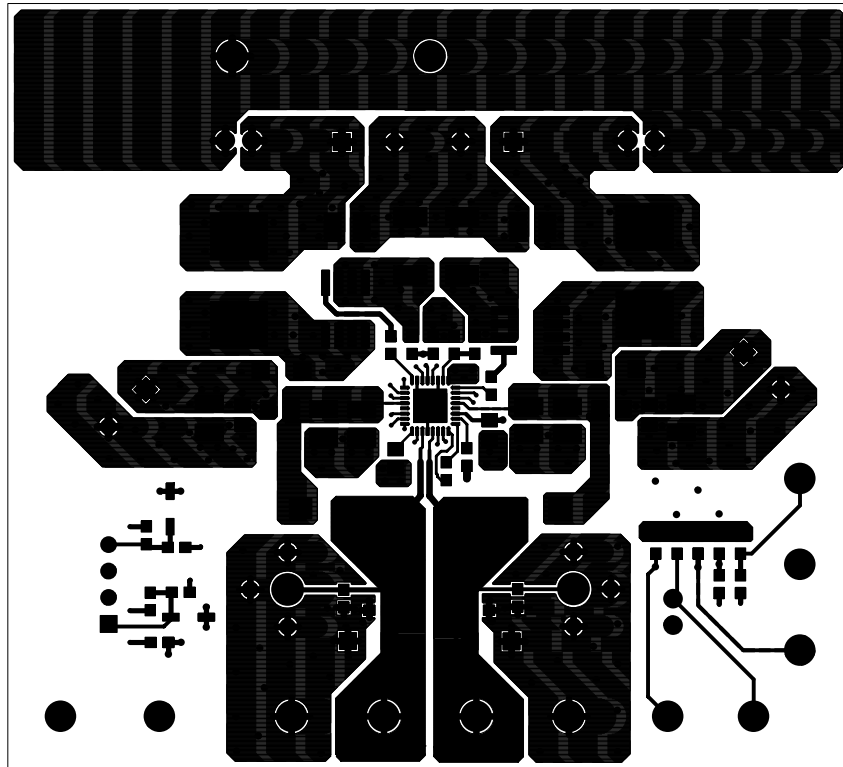


FIGURE 25. TOP LAYER COMPONENT SIDE

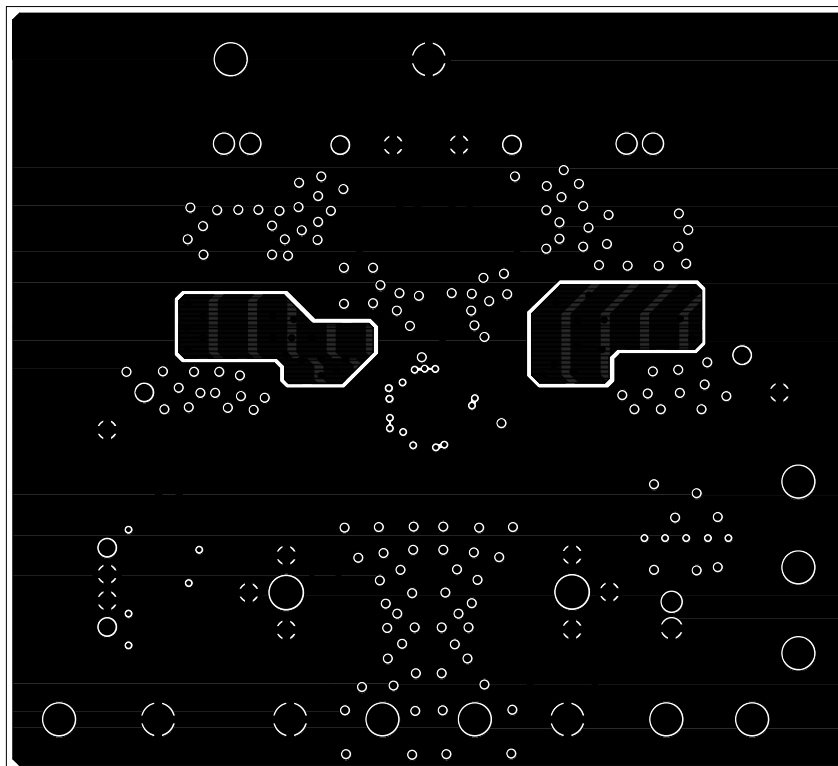


FIGURE 26. LAYER 2

ISL6424EVAL2 Layout (Continued)

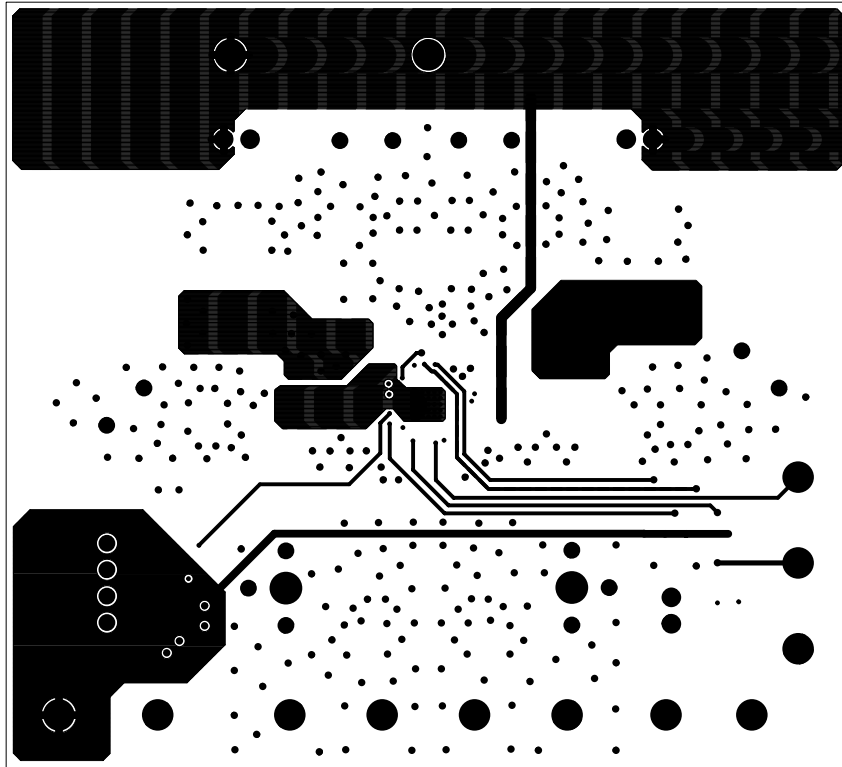


FIGURE 27. LAYER 3

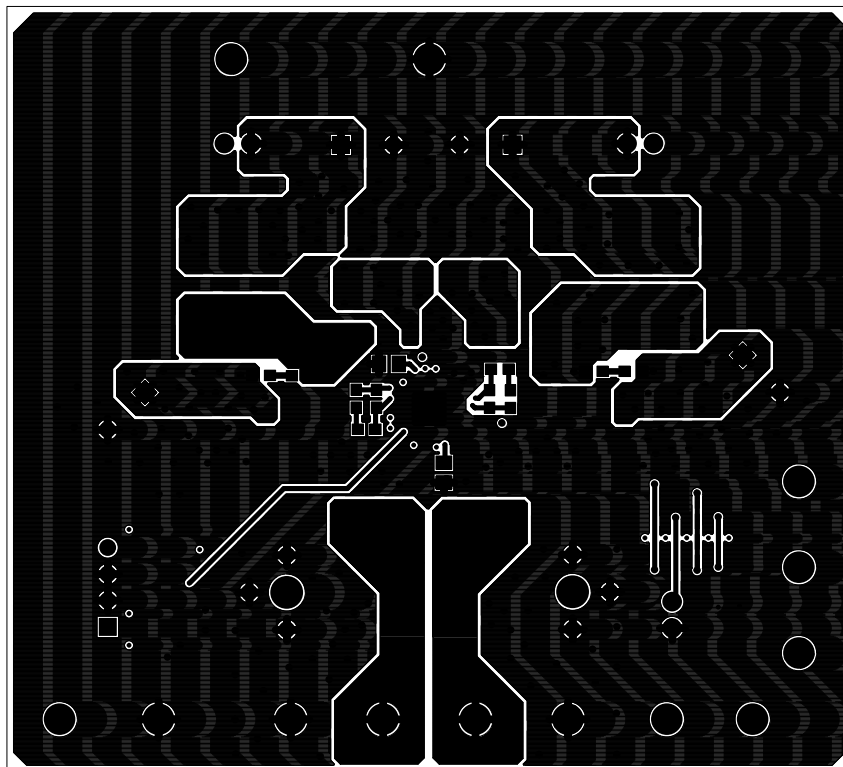


FIGURE 28. BOTTOM LAYER SOLDER SIDE

ISL6424EVAL2 Layout (Continued)

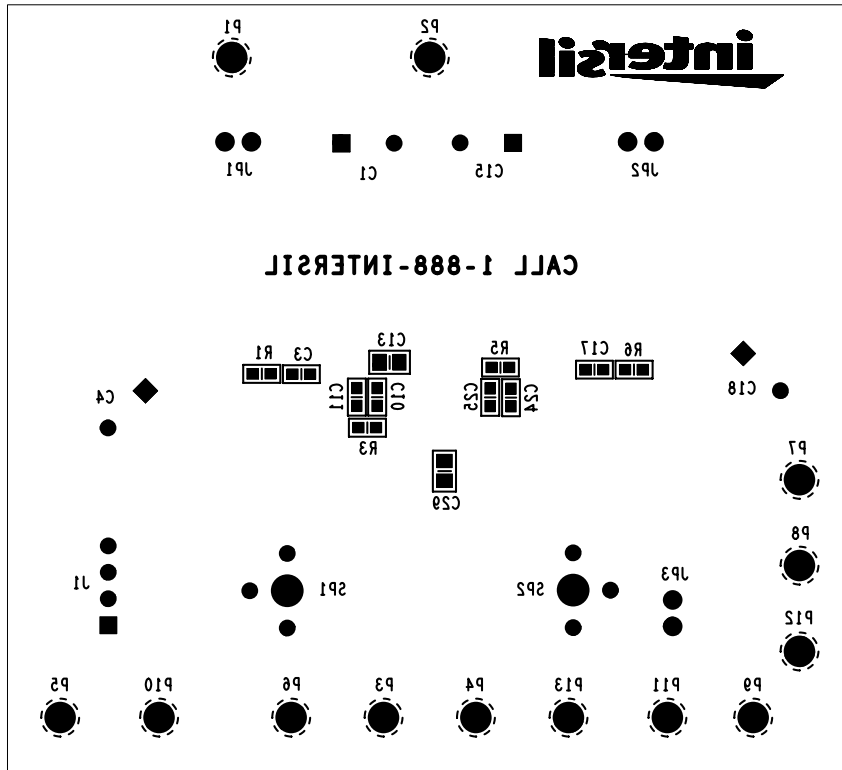


FIGURE 29. BOTTOM SILKSCREEN

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